

Conversion of Sulfinol-D to MDEA at the Shell Canada Burnt Timber Facility

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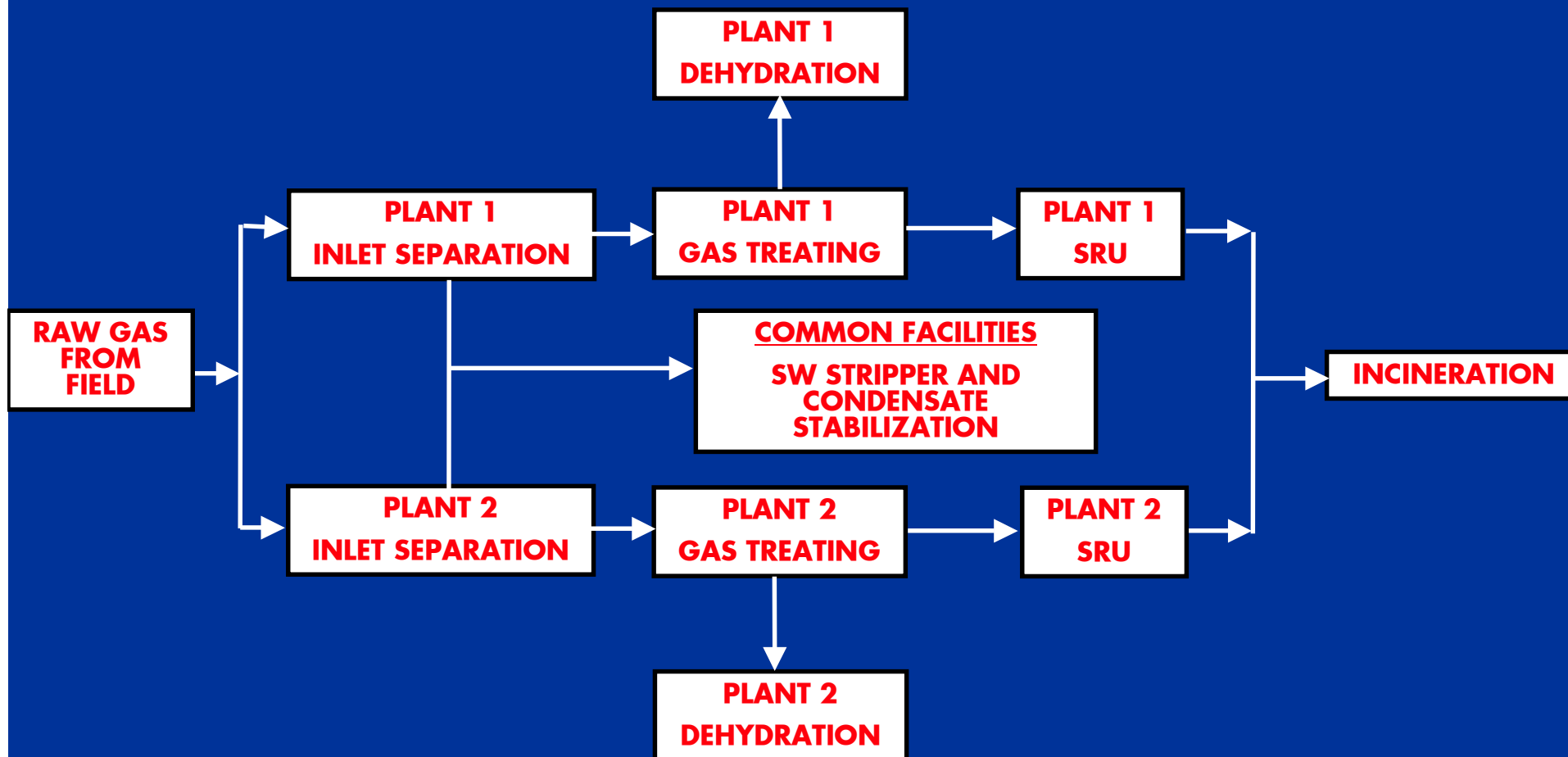
Introduction

- Shell Canada's Burnt Timber Facility is located 120 km northwest of Calgary, Alberta
- Plant 1 – constructed in 1970
 - Capacity of 1830 e3m3/d (65 MMSCFD)
- Plant 2 – constructed in 1976
 - Capacity of 2000 e3m3/d (71 MMSCFD)

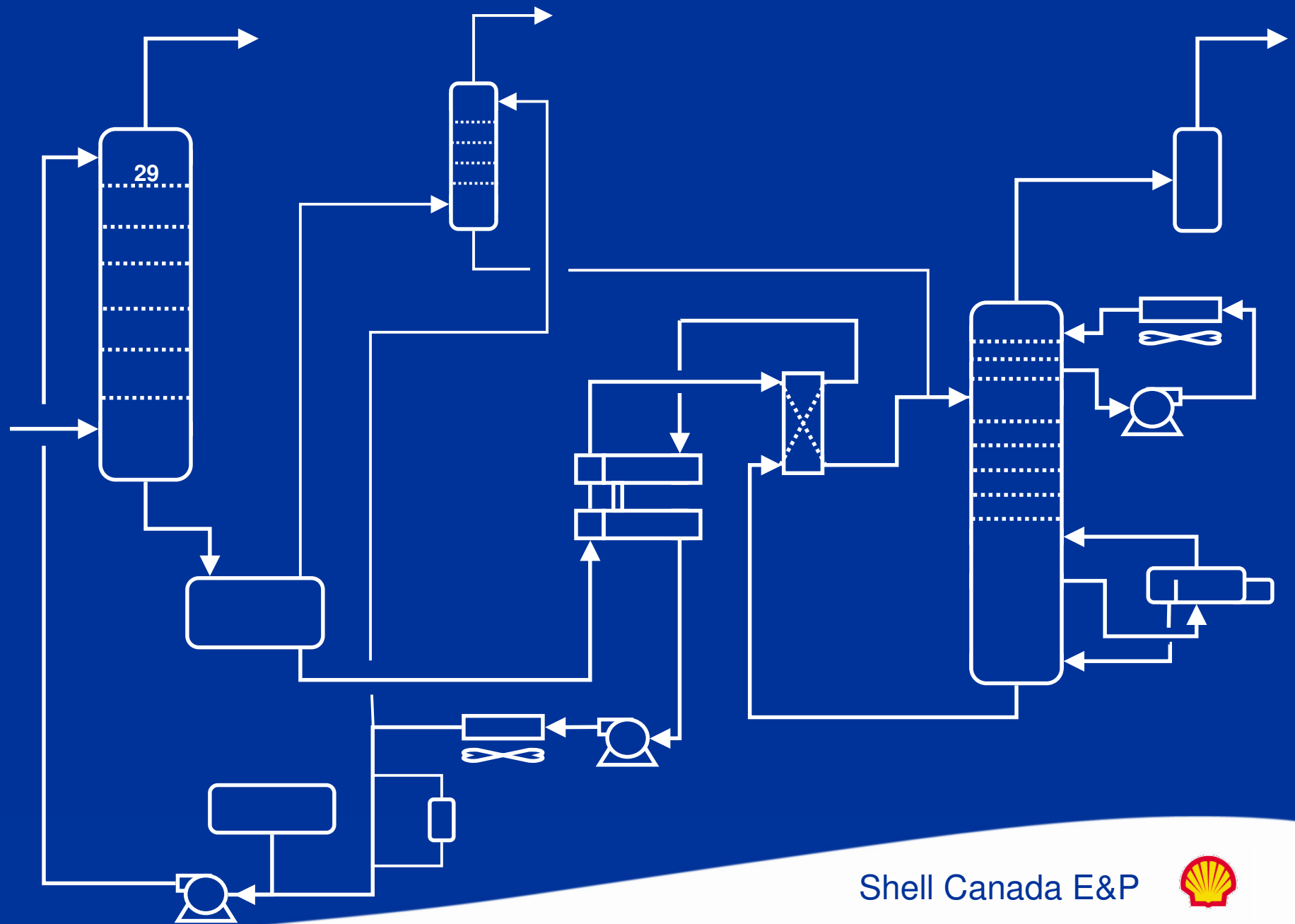




Current Plant Configuration



Original Gas Treating Configuration



Reasons for Change

- **Hydrocarbon Content in Acid Gas**
 - Consumption of air
 - Produced large amounts of CS_2
 - Un-combusted BTX caused deactivation of 1st converter bed
- **This resulted in 1st bed catalyst being changed every 6 to 9 months.**
 - Excessive operating costs
 - Lost Production



Reasons for Change

- **High CO₂ Content in Acid Gas**
 - **Increases pressure drop therefore reducing blower capacity and plant capacity**
 - **Production of COS reducing sulphur recovery**
 - **Reduces reaction furnace flame temperature**



Reasons for Change

- Change in feed gas composition
 - Burnt Timber Field: $\text{H}_2\text{S} = 10.2\%$ $\text{CO}_2 = 6.4\%$
 - Panther Field: $\text{H}_2\text{S} = 7\%$ $\text{CO}_2 = 11.5\%$

| Component (mole %) | Year | |
|-----------------------|------|------|
| | 2005 | 2020 |
| H_2S | 10.1 | 8.1 |
| CO_2 | 8.0 | 10.2 |
| N_2 | 0.6 | 0.5 |
| C1 | 75.8 | 80.4 |
| C2 | 2.1 | 0.8 |
| C3 | 0.4 | 0.2 |
| i-C4 | 0.1 | 0.0 |
| n-C4 | 0.1 | 0.0 |
| i-C5 | 0.1 | 0.0 |
| n-C5 | 0.1 | 0.0 |
| C6 | 0.3 | 0.1 |
| C7+ | 3.3 | 1.2 |



Reasons for Change

- **Changing Feed Composition would result in:**
 - **Poor Acid Gas $\text{H}_2\text{S}:\text{CO}_2$ ratio**
 - **Higher acid gas HC content due to higher amine circulation ratios**
- **End Result = Lower Plant capacity and lower sulphur recovery**



Benefits of Conversion to MDEA

- Slip CO₂ to sales improving acid gas H₂S:CO₂ ratio.
- Decrease HC co-absorption in the amine.
 - Decrease air requirements in SRU and increase capacity.
 - Increase heating value to sales gas.
 - Reduce flash gas volume.
- Circulation rate not impacted by H₂S:CO₂ ratio.
- Lower reboiler duty

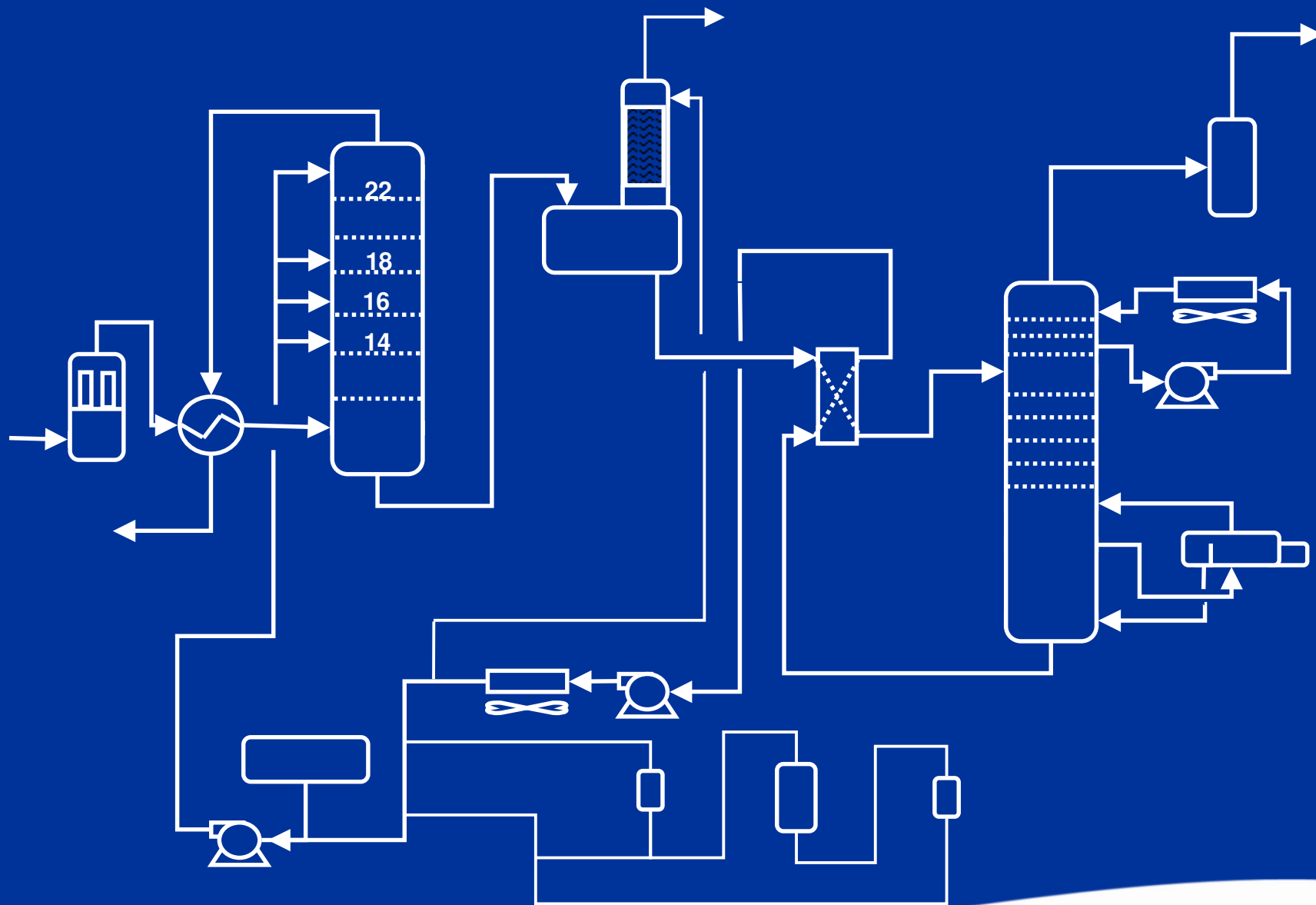


Risks of Conversion to MDEA

- **Reduced removal of trace sulphurs**
 - **Depending on raw gas trace sulphur content, may not be able to meet specification.**
- **Aqueous MDEA has a higher foaming tendency than Sulfinol which may lead to capacity constraints**
- **Decision was made to change amine to MDEA.**
- **Millenia Resource Consulting of Calgary was contracted to do the detailed Engineering design.**



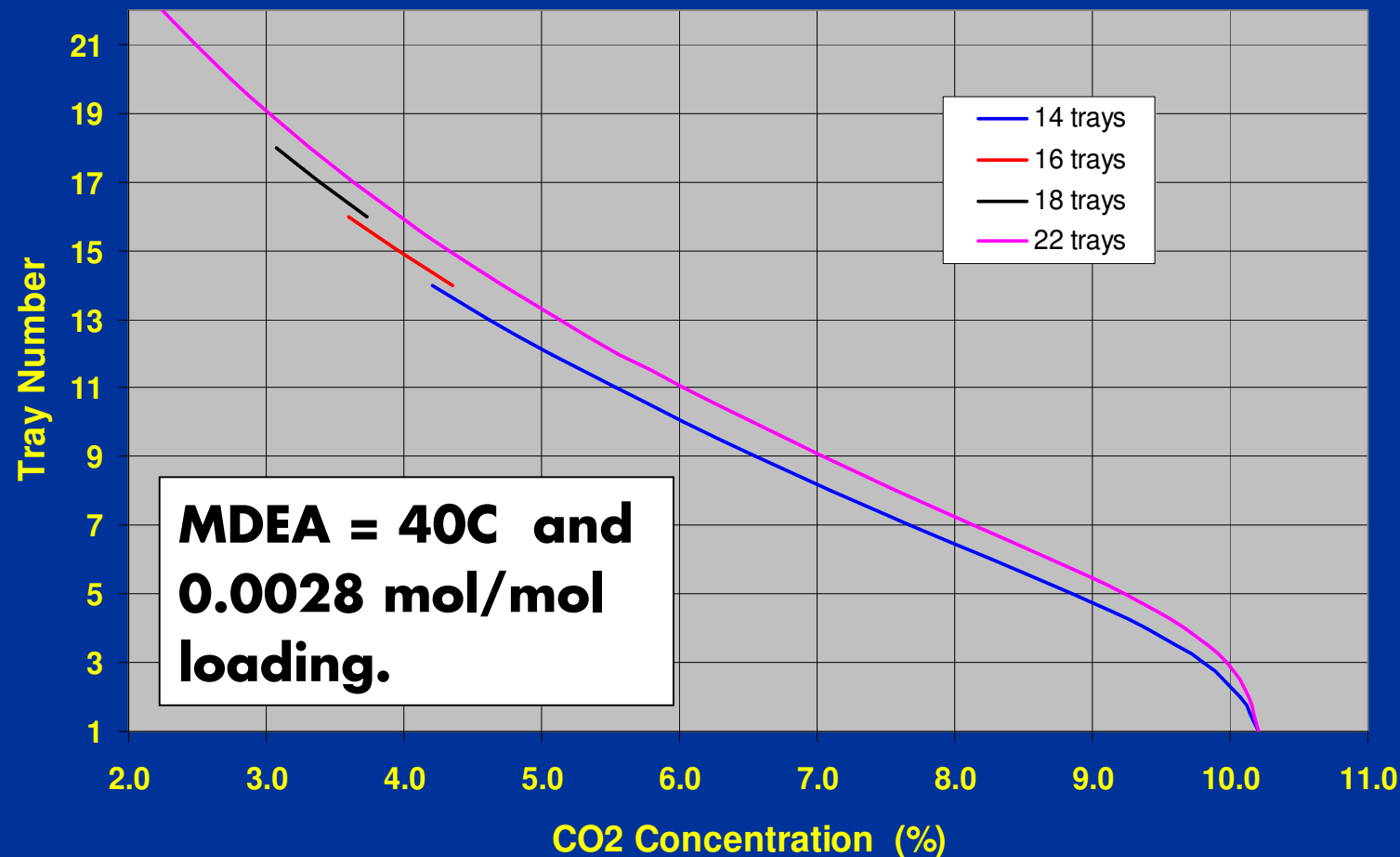
MDEA Conversion Modifications



Absorber Design

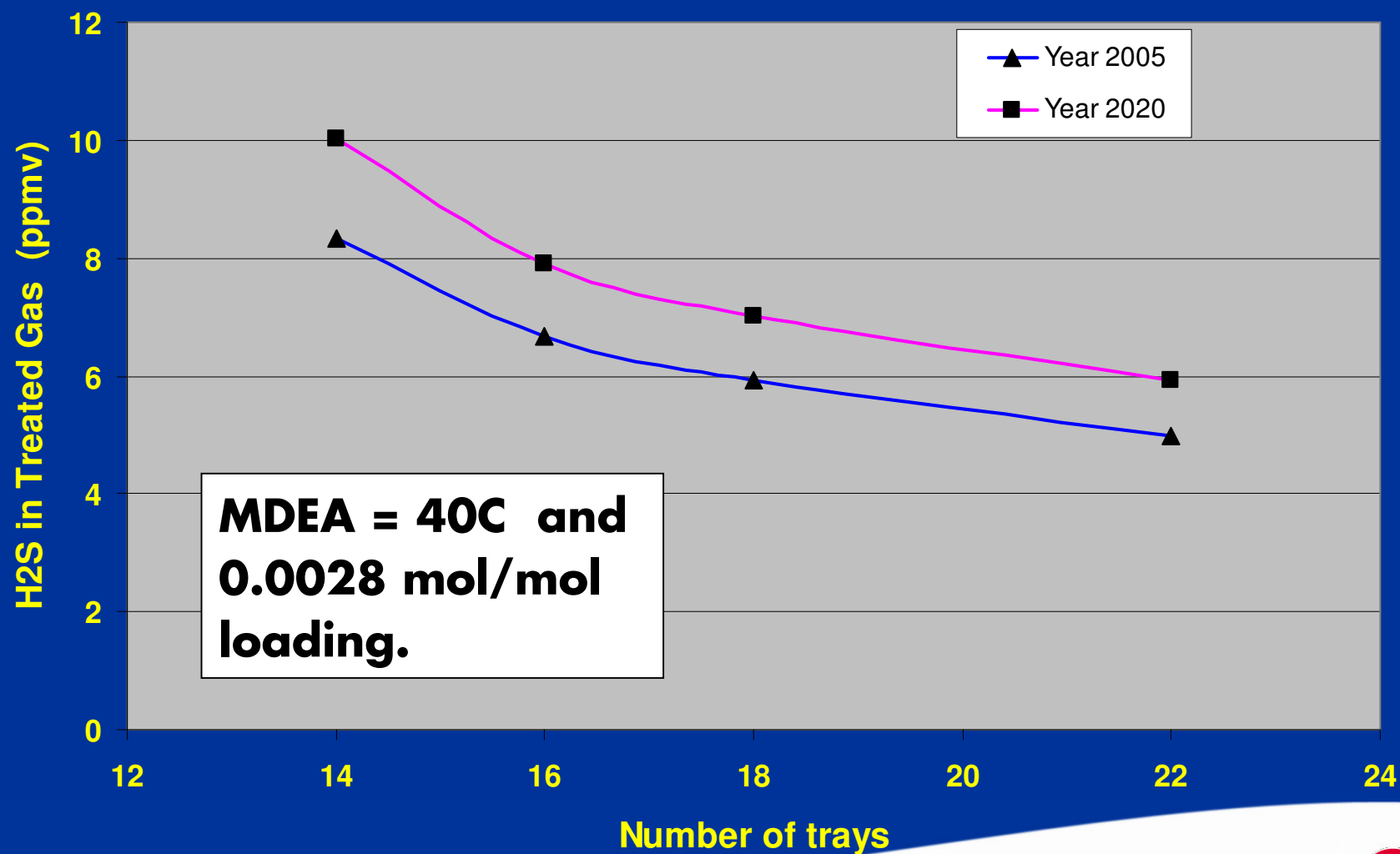
- Slip up to 4% CO₂ and less than 8 ppmv H₂S
- 2% CO₂ required when Plant 1 is shutdown

CO₂ Concentration Profile - Year 2020

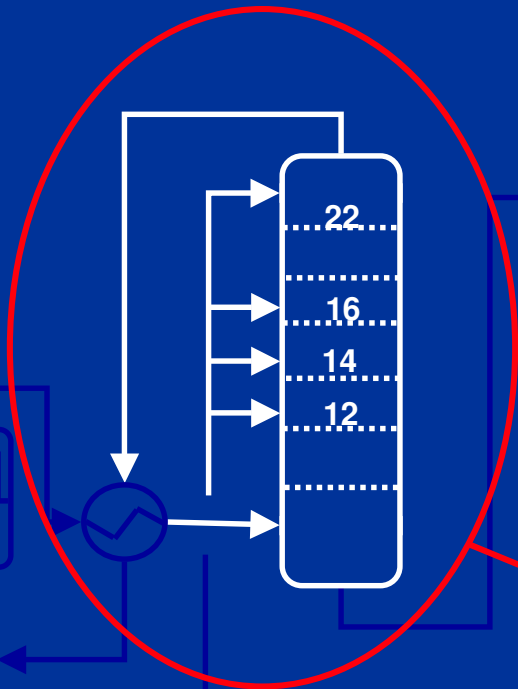


Absorber Design

H₂S vs Number of trays



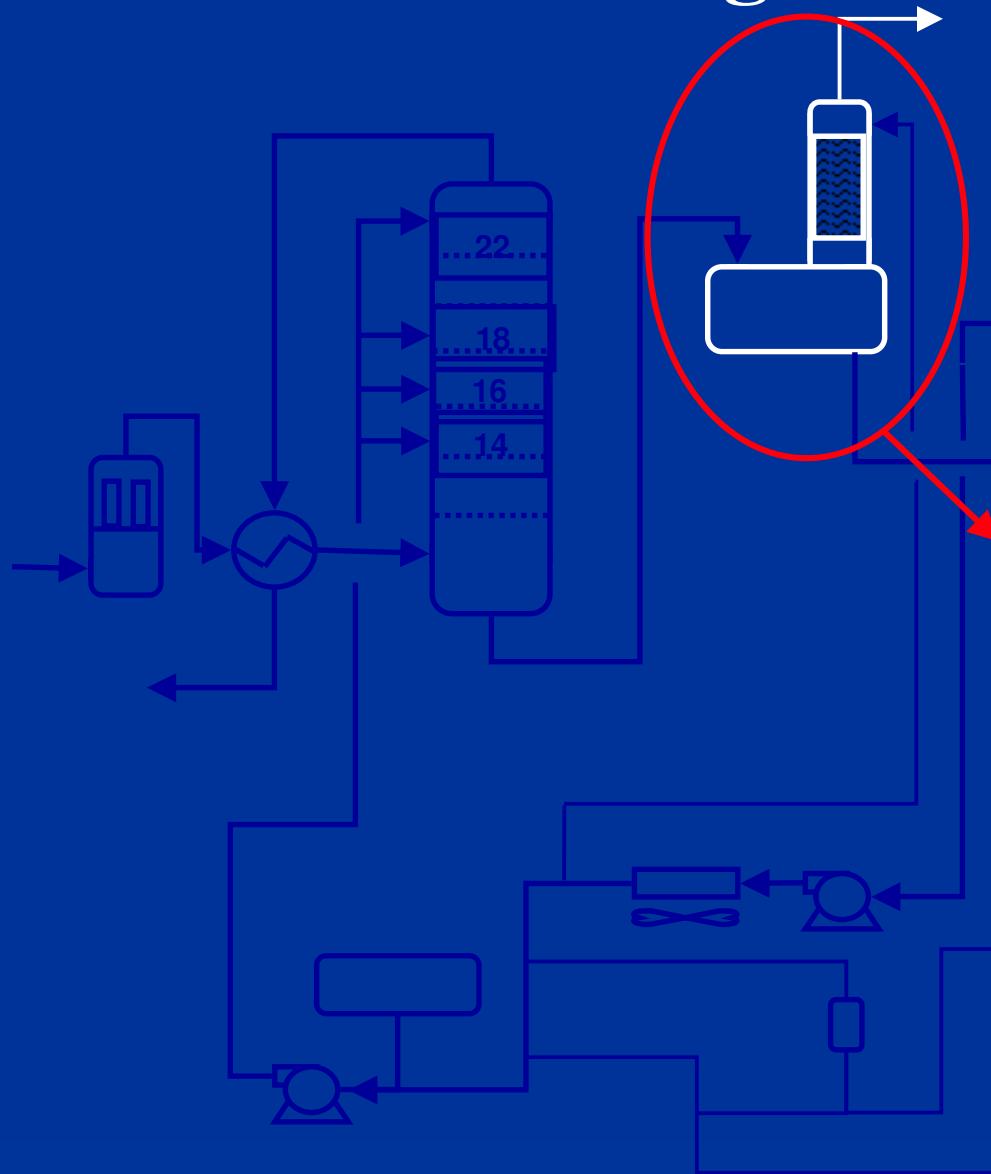
Absorber Design



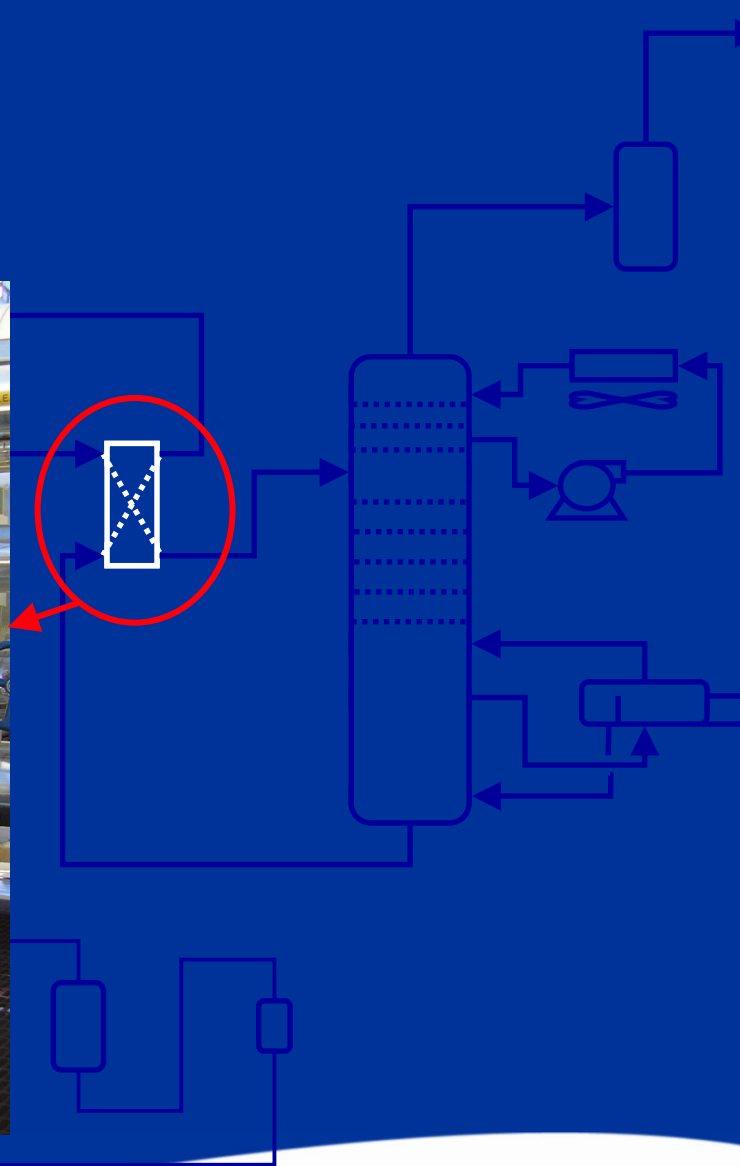
Shell Canada E&P



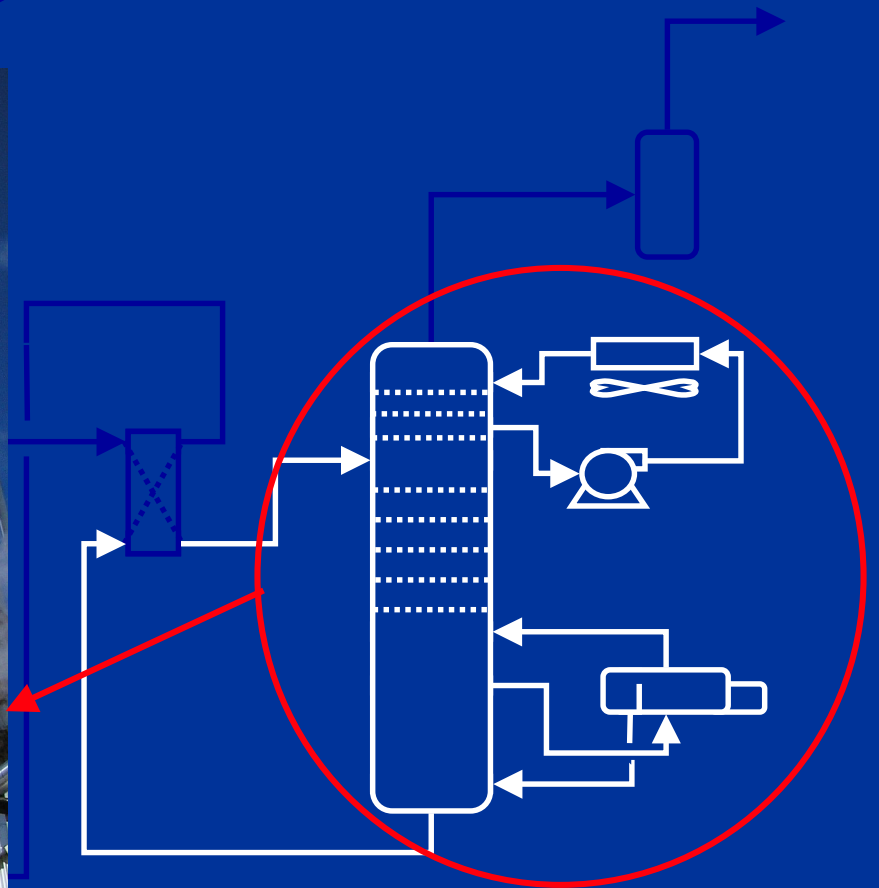
Flash Drum Design



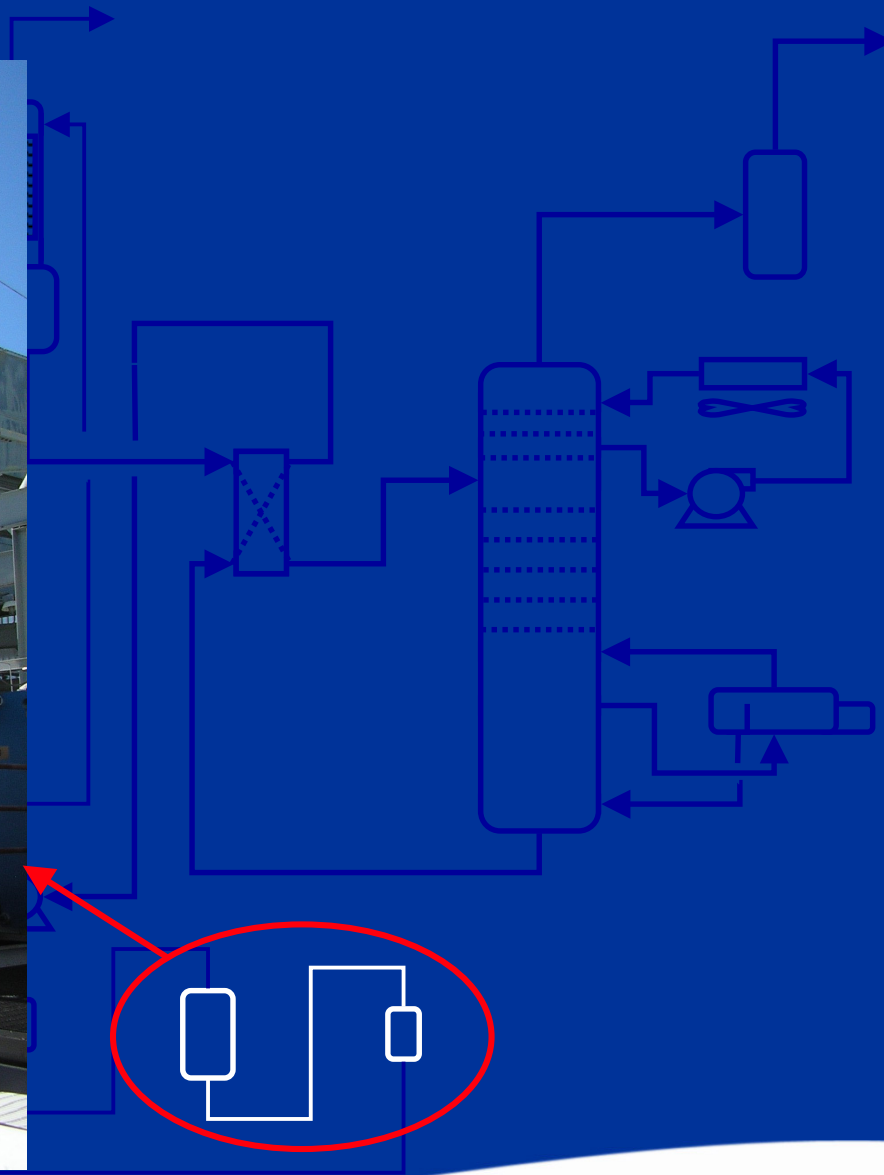
Lean Rich Exchangers



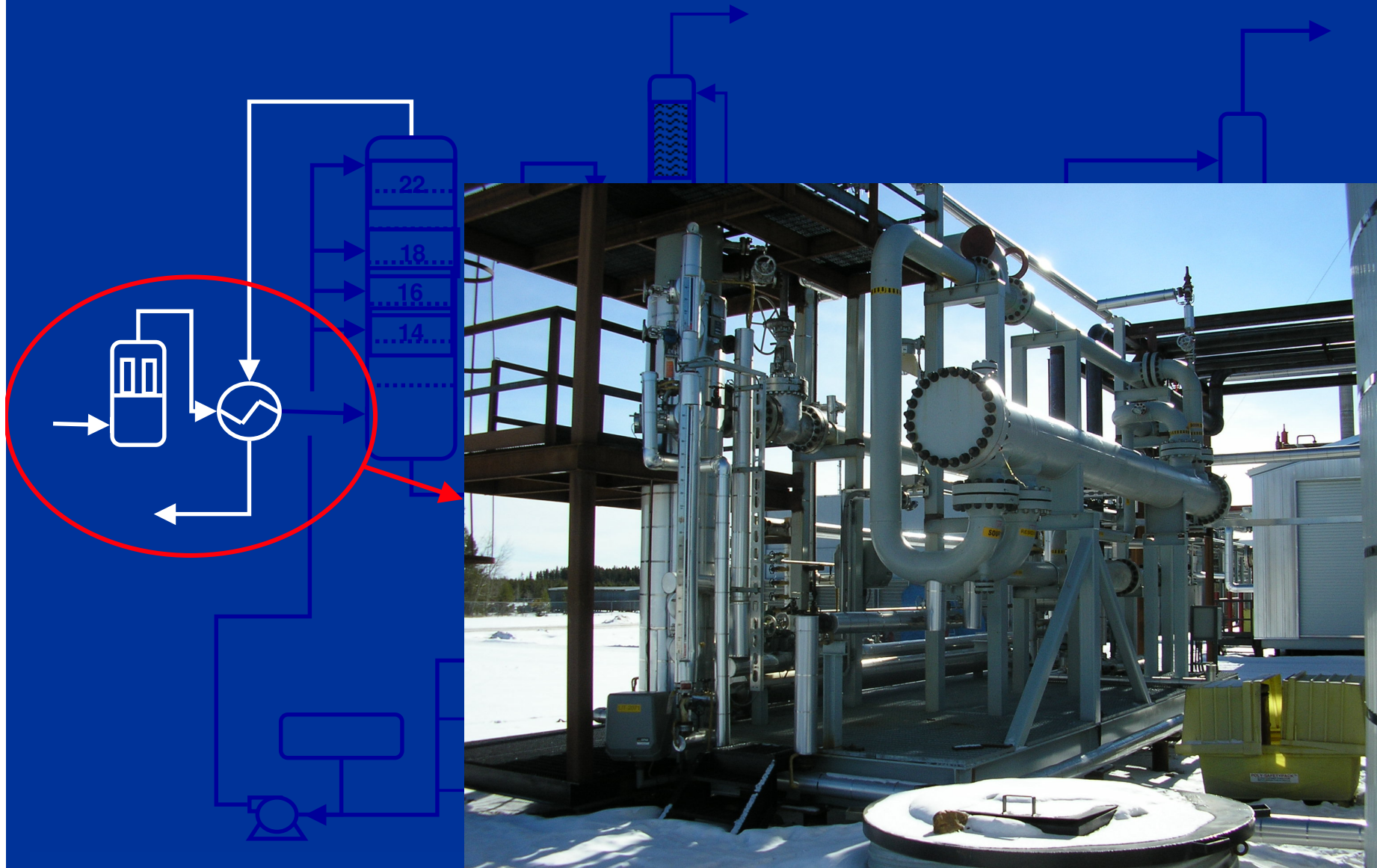
Regenerator



Carbon Filter



Inlet Filter Coalescer & Preheater



Construction

- Construction was one of the most challenging aspects of the project
- Equipment located on three skids
 - Gas/Gas Exchanger and Coalescer Skid
 - L/R Exchanger Skid
 - Flash Tank Skid
- Issues with the skids – late and unfinished.



Construction

- Major work during shutdown was in the Absorber
 - Installation of three feed nozzles
 - Installation/modification of tray rings
 - Strip lining the bottom 10 m
 - Lining the nozzles with stainless steel
- Absorber had to have a hydrogen bake out, continuous weld preheat, and stress relieving.



Commissioning, Start-up and Operation

- **First task was to clean the system**
 - **Absorber and regenerator were vacuumed.**
 - **Start-up suction strainers installed.**
 - **Vessels and piping were air freed and gross leak tested using N₂.**
 - **Final leak check at operating pressure with fuel gas.**



Commissioning, Start-up and Operation

- **Cleaning the system cont'd**
 - **System was charged with steam condensate.**
 - **Circulation was established with L/R exchangers by-passed.**
 - **Steam condensate temperature was raised to 60 deg C.**
 - **A degreasing solution was added (1% soda ash, 1% tri-sodium phosphate and 0.2% surfactant).**



Commissioning, Start-up and Operation

- **Cleaning the system cont'd**
 - **The system was completely drained and then refilled with fresh steam condensate.**
 - **Circulation was then established for 3 hours or 3 full circulations.**
 - **The system was drained then charged with 50:50 MDEA/Water mixture.**



Commissioning, Start-up and Operation

- **Start-up**

- Gas was introduced with no unexpected issues.
- When L/R exchangers were placed in series, the Booster Pumps experienced cavitation.
- The pumps were damaged and 3 day outage was necessary due to delivery of replacement parts.



Commissioning, Start-up and Operation

- **Start-up....Next Problem**
 - **Plugged Absorber Level Control Valve.**
 - **Valve was plugged with welding slag, bolts, and other debris.**
 - **This occurred three more times with the same result.**
 - **Installed a bypass LCV with different style trim.**



Commissioning, Start-up and Operation

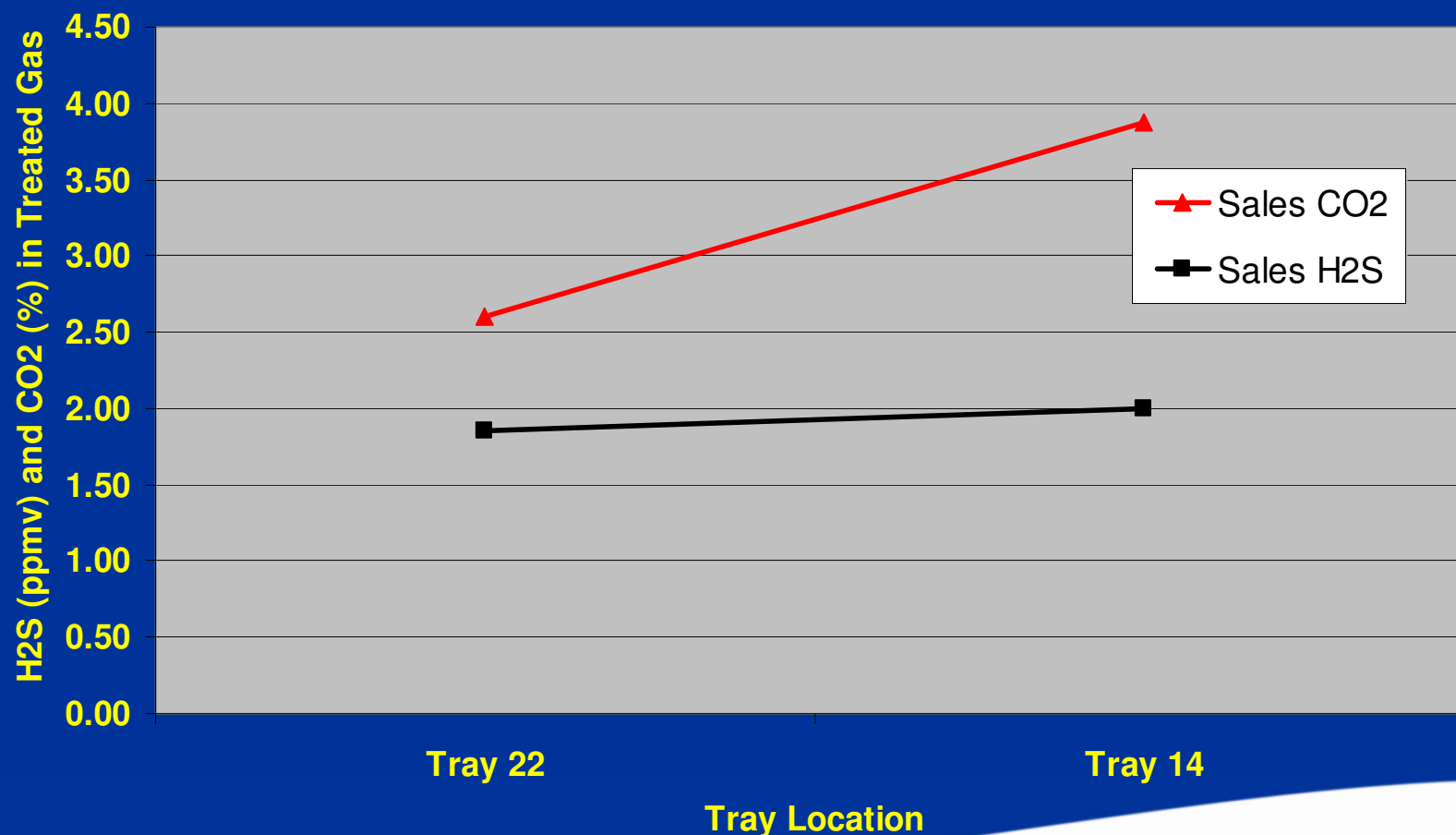
- **Start-up**

- Hang-ups were experienced in the regenerator due to excessive steaming
- Placing L/R exchangers in series on the rich side solved this issue.
- The L/R exchangers did experience some plugging.
- They were cleaned several times online.



Optimization and Current Operation

H2S and CO2 in Treated Gas versus Tray Location



Key Process Performance Results

- Inlet Raw Gas
 - Design = 1850 e3m3/d
 - Performance Test = max. 2050 e3m3/d
- Reboiler Steam demand
 - 25% less steam per volume of raw gas
- Flash Gases
 - Reduced from 30 to 2-4 e3m3/d



Key Process Performance Results

- Sulphur Plant Operation

| Parameter | Sulfinol | MDEA |
|--|----------------------------|----------------------------|
| Acid Gas H ₂ S | 58% | Up to 70% H ₂ S |
| Acid Gas HC Content | 2.5% (CH ₄ eq.) | <1% (CH ₄ eq.) |
| BTX in Acid Gas | > 2300 ppmv | 400 – 500 ppmv |
| CS ₂ to 1 st Converter | 1.25% | 0.23% |
| COS & CS ₂ from Stack | 130 & 200 ppmv | 50 & 16 ppmv |
| TRS (Total Reduced S) | 600 ppmv | 100 ppmv |
| Sulphur Recovery | 95% | 96.9% |



Key Process Performance Results

- Trace Sulphur Removal

| | Inlet Gas | % Removal | |
|--|-------------------------|-----------|-----|
| | | COS | RSH |
| Design (MDEA) | 117 mg S/m ³ | 28% | 37% |
| MDEA | 112 mg S/m ³ | 26% | 47% |
| Sulfinol | 112 mg S/m ³ | 85% | 80% |
| Total Sulphur in Sales = 59 mg S/m ³ (spec = 115) | | | |



Key Process Performance Results

- **Trace Sulphur Removal**
 - Subsequent tests showed only 8% and 15% removal of COS and RSH with the inlet containing 199 mg S/m³.
 - Combined Sales contained = 141 mg S/m³
 - Inlet Trace Sulphur was high due to sulphur washes on a sulphur producing well.



Summary

- **Conversion to MDEA was a success at Burnt Timber.**
- **System operates well with little foaming.**
 - **Inlet coalescer and carbon bed.**
- **MDEA was the correct solution to the problem at Brunt Timber.**

